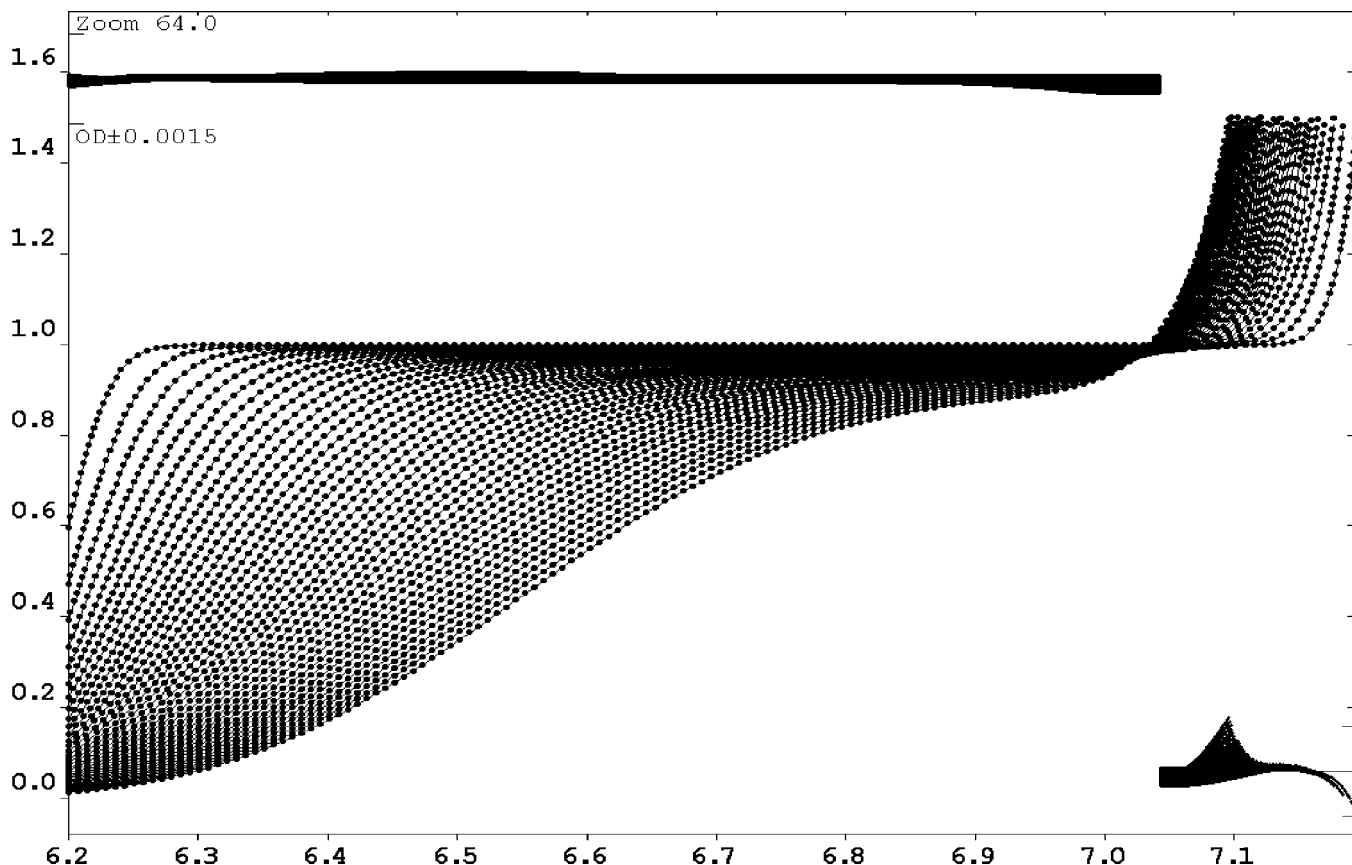


Lamm



LAMM (N = correct air + bottom boundary) (absorption) Date: 9:2:2004
 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27
 28 29 30 31 32 33 34 35 36 37 38 39 40
 Ext=1.000;Ampl:1.000 R-RASTER: 1.00E-03 T-RASTER:1.00 start time: 400
 Noise=0.0000 S=2.00 D=10.00 Rm=6.2000 Rb=7.2000 time differ.: 400
 C:\temp\091503\085340\00041

Parameter(total/estimated)/tau(last set)	7/ 6	1.1208E-01
Data points/files/time offset/TI-noise	37108/ 40 0	FALSE
Cell,temperature,wavelength,rotor:rpm,rpc	9 20.0 220	40000 1
Iterations/faulted/part.spec.vol./load.conc	3/ 0 0.7360	FALSE
Maximal iterations/OD-max/slit speed(mm/sec)	200 1.50	0.0000
Radius range/rpm/Calc. last bottom point	6.2000/7.1940	40000 N
Test for validity<1/no.of data file/RI-noise	0.136 40	FALSE
Cancel outliers/start time(s)/TI-noise subtract. N	400	FALSE
Standard deviation(rmsd)/time diff./SSR	0.00015 400	8.8475E-04
Damping parameter,start / epsilon	1.5181 5.00	1.4871E-02

PARAMETER	VALUE	STD.DEVIATION	START VALUES
Initial absorbance	1.0016E+00	4.0204E-06	9.9403E-01
Svedberg coeff. (Svedb.units)	1.9963E+00	1.0932E-05	1.9737E+00
Base line	-1.4575E-03	3.9617E-06	0.0000E+00
Meniscus radius	6.2000E+00	9.3254E-07	6.2000E+00
Bottom radius	7.2001E+00	6.7210E-07	7.1940E+00
Rotation parameter	0.0000E+00		0.0000E+00
Diffusion coefficient	1.0011E-06	1.0589E-11	7.5099E-07
Molecular mass/stdv/(psv*rho)	1.8413E+04	2.1931E-01	7.3600E-01
Stokes radius(water) (m)/excluded volume(L/g)		2.1260E-09	5.2681E-03
Water thicknis from stokes radius(m)//-Vol/g		3.7485E-10	5.8102E-01
Friction ratio/viscosity/rho	1.2141E+00	1.0086E+00	1.0000E+00
Archibald mass at meniscus/bottom (1.File)		1.8406E+04	1.8420E+04

The program LAMM

The program **LAMM** contains 9 model functions. The first four equations (**P**, **S**, **H**, **R**) are suitable for synthetic boundary experiments. The so-called diffusion time τ_d implemented in the XLA (I) output can be used by choice. The diffusion time works in the divisors of the error functions containing the diffusion coefficient (by function **R** only in the first error function),

$$\sqrt{\varepsilon\tau} = \frac{2}{r_m} \sqrt{Dt} \quad \text{and} \quad \sqrt{\varepsilon(e^{\tau_d} - 1)}$$

but not in the transport terms, the numerator of the error functions. Tests with synthetic traces (Claverie) have shown that this statement can well describe a pure diffusion process.

Function P. Fujita 1975, Eq.2.127

$$c_r = \frac{c_0 e^{-\tau}}{2} \operatorname{erfc}\left(\frac{z - \tau}{2\sqrt{\varepsilon\tau}}\right), \quad z = 2\ln\left(\frac{r}{r_m}\right), \quad \tau = 2\omega^2 st, \quad \varepsilon = \frac{2D}{s\omega^2 r_m^2} \quad (1)$$

Function S. Fujita 1962, Eq.2.191 With consideration of concentration dependent sedimentation.

$$x = \frac{r^2}{r_m^2}, \quad g = \sqrt{1 - \alpha(1 - e^{-\tau})}, \quad \varepsilon = \frac{2D}{s_0\omega^2 r_m^2}, \quad s_c = s_0 \left(1 - \alpha \frac{c}{c_0}\right)$$

$$c_r = \frac{c_0 e^{-\tau}}{g^2 \sqrt{x}} \frac{(\sqrt{x} - 0.25\varepsilon(e^{\tau/2} - e^{-\tau/2})) \operatorname{erfc}(p) e^{p^2} + g\sqrt{\varepsilon(e^{\tau} - 1)}/\pi}{e^{p^2} (2 - \operatorname{erfc}(p)) + g \operatorname{erfc}(\xi) e^{\xi^2}} \quad (2)$$

$$\xi = \frac{e^{\tau/2} - \sqrt{x} + 0.25\varepsilon(e^{\tau/2} - e^{-\tau/2})}{\sqrt{\varepsilon(e^{\tau} - 1)}}, \quad p = \frac{g^2 e^{\tau/2} - \sqrt{x} + 0.25\varepsilon(e^{\tau/2} - e^{-\tau/2})}{g\sqrt{\varepsilon(e^{\tau} - 1)}}$$

Function H. According to Hiester and Vermeulen (Fujita 1975, Eq. 2.167). This is a very accurate formula.

$$c_r = \frac{c_0 e^{-\tau}}{2} \left\{ \operatorname{erfc}(\xi) + \frac{\sqrt{2\varepsilon \sinh(\tau/2)}}{x^{1/4} \left[1 + (xe^{-\tau})^{1/4}\right] \sqrt{\pi}} e^{-\xi^2} \right\} \quad (3)$$

The symbols have the same meaning as in Eq.2.

The next function is also suitable for synthetic boundary but with consideration of **bottom boundary**. It follows from function **N** (see later) without terms 2 and 3 responsible for the meniscus boundary.

Function R

$$\begin{aligned} \frac{2ce^\tau}{c_0} = \operatorname{erfc} \left(\frac{e^{\tau/2} - 0.5w + 0.25\varepsilon(e^{-\tau/2} - e^{\tau/2})}{\sqrt{\varepsilon(e^\tau - 1)}} \right) \\ - \operatorname{erfc} \left(\frac{-z + d\tau}{2\sqrt{\varepsilon_b\tau}} \right) - \frac{1}{1-d} \exp \left(\frac{dz}{\varepsilon_b} \right) \operatorname{erfc} \left(\frac{-z - d\tau}{2\sqrt{\varepsilon_b\tau}} \right) \\ + \frac{2-d}{1-d} \exp \left(\frac{(1-d)\tau + z}{\varepsilon_b} \right) \operatorname{erfc} \left(\frac{-z - (2-d)\tau}{2\sqrt{\varepsilon_b\tau}} \right) \end{aligned} \quad (4)$$

For definition of the symbols see function N.

The next four model functions (**D**, **O**, **C**, **M**) are suitable for standard double sector cells with consideration of meniscus boundary. The last function (**M**) considers additionally the concentration dependence of sedimentation coefficient.

Function D. Philo 1997 developed an improved form of the Fujita-MacCosham equation.

$$c_r = \frac{c_0 e^{-\tau}}{2} \left\{ \operatorname{erfc}(p(1 + \alpha\tau)) - 2\sqrt{\frac{\tau}{\pi\varepsilon}} e^{-p^2(1 + \beta\varepsilon\tau)} + \left(1 + \frac{\tau + \ln x}{\varepsilon}\right) \operatorname{erfc}\left(\frac{\tau + \ln x}{\sqrt{4\varepsilon\tau}}\right) e^{\left(\frac{\ln x}{\varepsilon}\right)} \right\} \quad (5)$$

$$p = \frac{\tau - \ln x}{\sqrt{4\varepsilon\tau}}, \quad \alpha = 0.2487, \quad \beta = 2, \quad \varepsilon = \frac{2D}{s\omega^2 r_m^2}$$

Function O. This is an equation developed by Holladay 1979.

$$c_r = \frac{c_0}{2} e^{-\tau} \left\{ \operatorname{erfc}\left(\frac{\tau\alpha - z}{2\sqrt{a\varepsilon\tau}}\right) - \frac{a}{\varepsilon} \exp\left(\frac{z\alpha}{a\varepsilon}\right) \operatorname{erfc}\left(\frac{\tau\alpha + z}{2\sqrt{a\varepsilon\tau}}\right) + \frac{\gamma}{\varepsilon} \exp\left(\tau + \frac{z}{\varepsilon}\right) \operatorname{erfc}\left(\frac{\tau\gamma + z}{2\sqrt{a\varepsilon\tau}}\right) \right\} \quad (6)$$

$$\alpha = a - \varepsilon, \quad \gamma = a + \varepsilon, \quad z = \left(\frac{r}{r_m}\right)^2 - 1, \quad a = \frac{e^\tau - 1}{\tau}$$

Function C: This is the best function to analyze experiments obtained in standard double sector cells and considering the meniscus boundary condition only (Behlke and Ristau 2002).

$$\begin{aligned} \frac{2ce^\tau}{c_0} = \operatorname{erfc} & \left(\frac{e^{\tau/2} - 0.5w - 1 + 0.25\varepsilon(e^{-\tau/2} - e^{\tau/2})}{\sqrt{\varepsilon(e^\tau - 1)}} \right) \\ & - \frac{1}{(1-b)} \exp\left(\frac{bw}{\varepsilon}\right) \operatorname{erfc}\left(\frac{w + 2b(e^{\tau/2} - 1)}{2\sqrt{2\varepsilon(e^{\tau/2} - 1)}}\right) \\ & + \frac{(2-b)}{(1-b)} \exp\left(\frac{w + 2(e^{\tau/2} - 1)(1-b)}{\varepsilon}\right) \operatorname{erfc}\left(\frac{w + 2(2-b)(e^{\tau/2} - 1)}{2\sqrt{2\varepsilon(e^{\tau/2} - 1)}}\right) \end{aligned} \quad (7)$$

$$w = 2\left(\frac{r}{r_m} - 1\right), \quad b = 1 - \varepsilon/2$$

Funktion M. This variant is developed for concentration dependent sedimentation. It combines the Fujita-formula S with the last two terms of function C but with slightly changed time terms (only τ instead of $2(\exp(\tau/2)-1)$). This model function is suitable to study the concentration dependence of sedimentation coefficient from concentration profiles with sufficient plateau region.

$$\begin{aligned} c_r = \frac{c_0 e^{-\tau}}{g^2 \sqrt{x}} & \frac{(\sqrt{x} - 0.25\varepsilon(e^{\tau/2} - e^{-\tau/2})) \operatorname{erfc}(p) e^{p^2} + g\sqrt{\varepsilon(e^\tau - 1)}/\pi}{e^{p^2}(2 - \operatorname{erfc}(p)) + g \operatorname{erfc}(\xi) e^{\xi^2}} \\ & + \frac{c_0 e^{-\tau(1-\alpha)}}{2} \left\{ -\frac{1}{(1-b)} \exp\left(\frac{bw}{\varepsilon}\right) \operatorname{erfc}\left(\frac{w + 2b(e^{\tau/2} - 1)}{2\sqrt{2\varepsilon(e^{\tau/2} - 1)}}\right) \right. \\ & \left. + \frac{(2-b)}{(1-b)} \exp\left(\frac{w + 2(e^{\tau/2} - 1)(1-b)}{\varepsilon}\right) \operatorname{erfc}\left(\frac{w + 2(2-b)(e^{\tau/2} - 1)}{2\sqrt{2\varepsilon(e^{\tau/2} - 1)}}\right) \right\} \end{aligned} \quad (8)$$

$$x = \frac{r^2}{r_m^2}, \quad \varepsilon = \frac{2D}{s_0 \omega^2 r_m^2}, \quad w = 2\left(\frac{r}{r_m} - 1\right)(1 + 0.475\alpha)$$

$$s_c = s_0 \left(1 - \alpha \frac{c}{c_0}\right), \quad g = \sqrt{1 - \alpha(1 - e^{-\tau})}, \quad b = 1 - \frac{\varepsilon}{2}$$

$$\xi = \frac{e^{\tau/2} - \sqrt{x} + 0.25\varepsilon(e^{\tau/2} - e^{-\tau/2})}{\sqrt{\varepsilon(e^\tau - 1)}}, \quad p = \frac{g^2 e^{\tau/2} - \sqrt{x} + 0.25\varepsilon(e^{\tau/2} - e^{-\tau/2})}{g\sqrt{\varepsilon(e^\tau - 1)}}$$

The supplement factor to w (pure α -relations) is an empirical improvement.

Function N is a whole boundary solution for normal standard sector cells according to Behlke and Ristau 2002.

$$\begin{aligned}
\frac{2ce^\tau}{c_0} = & \operatorname{erfc} \left(\frac{e^{\tau/2} - 0.5w - 1 + 0.25\varepsilon(e^{-\tau/2} - e^{\tau/2})}{\sqrt{\varepsilon(e^\tau - 1)}} \right) \\
& - \frac{1}{(1-b)} \exp \left(\frac{bw}{\varepsilon} \right) \operatorname{erfc} \left(\frac{w + 2b(e^{\tau/2} - 1)}{2\sqrt{2\varepsilon(e^{\tau/2} - 1)}} \right) \\
& + \frac{(2-b)}{(1-b)} \exp \left(\frac{w + 2(e^{\tau/2} - 1)(1-b)}{\varepsilon} \right) \operatorname{erfc} \left(\frac{w + 2(2-b)(e^{\tau/2} - 1)}{2\sqrt{2\varepsilon(e^{\tau/2} - 1)}} \right) \\
& - \operatorname{erfc} \left(\frac{-z + d\tau}{2\sqrt{\varepsilon_b\tau}} \right) - \frac{1}{1-d} \exp \left(\frac{dz}{\varepsilon_b} \right) \operatorname{erfc} \left(\frac{-z - d\tau}{2\sqrt{\varepsilon_b\tau}} \right) \\
& + \frac{2-d}{1-d} \exp \left(\frac{(1-d)\tau + z}{\varepsilon_b} \right) \operatorname{erfc} \left(\frac{-z - (2-d)\tau}{2\sqrt{\varepsilon_b\tau}} \right)
\end{aligned} \tag{9}$$

$$b = 1 - \varepsilon/2, \quad w = 2 \left(\frac{r}{r_m} - 1 \right), \quad d = 1 - \varepsilon_b/2$$

$$z = 2 \frac{r}{r_b} \left(1 + a\varepsilon(e^{\tau/2} - 1) \right) - 2$$

$$\varepsilon_b = \frac{2D}{r_b^2 s \omega^2} \left(1 + c\varepsilon(e^{\tau/2} - 1) \right)$$

The first 3 terms are identical with function **C**. The quantities a and c are pure empirical improvements for the bottom part.

$$a = \frac{9.107}{p} \exp(-\ln(p)(0.1783 \ln(p) - 1)) + 2.4917$$

$$p = 1 + 84.08(\varepsilon - 0.01234)$$

$$c = \frac{0.2713}{h} \exp(-\ln(h)(0.02147 \ln(h) - 1)) - 0.091$$

$$h = 1 + 455.75(\varepsilon - 0.002539)$$

The program LAMM is written for window systems with a graphic resolution of 800*600 pixels or higher. The program can fit maximal 700 concentration profiles simultaneously. One file can contain maximal 2800 data points. Some windows variants needs the system option "border line automatically in the back ground" else the border line can appear on the graphic screen.

The program reads XLA-Files in the old or new version and also the interference files of the XLI.

The organization of the file input is oriented on the output of the XLA/I. That means at first the program reads the date of the experiment as subdirectory and than the subdirectory named by the time of experiment in which the actual data files are stored. Therefore after the file type is chosen (absorption or interference) and some useful program options are passed the **device** (with pathway) and the name of the folder which contain the date subdirectories must be given. The wanted one is chosen by a mouse click. A list with the time directories is now presented and the wanted is again selected by a mouse click. The data files can be loaded all simultaneously or step by step. They are shown in a graphic on the monitor screen. In the first mode the wanted part of the files and the meniscus and bottom radii are given in for all together whereas in the second mode the meniscus and bottom radius is given in at the first concentration profile loaded but the wanted part for fit can be chosen separately for each data file. The corresponding radii are chosen by moving the cross hairs to the wanted radial value. The crosshairs will be moved by the mouse with simultaneously pressing the left button. The cross-hairs can alternatively moved with the arrow keys on the keyboard. By simultaneously pressing the shift key you can accelerate the moving. Press now the key **A** for the wanted start radius and **E** for the end radius of the fitting region, respectively. Additionally the meniscus position and the bottom position have to inspire by pressing the key **M** (meniscus) and **B** (bottom). By other model functions as N the bottom position is a dummy parameter. In the one by one mode the program loads successively all files but the meniscus and bottom radius must be inspired only at the first trace. Furthermore you can finish untimely the further loading of data files by pressing the keys A and E at the same radius position. For the fit of Faxen type model functions it is possible to cut up the traces by input of the wanted radius position. The cutted data points are stored and can reactivated.

To enable the reading of data sets in the new XLA version made with more than one wavelength it is possible to choose the start file and the following sequence. If p.e. records are made at three wavelengths each 3. data file has the same wavelength. The start file determine the wavelength for the following files.

In the new data file mode of the XLA it is possible to determine the loading concentration (absorption) from the 3000-rpm data file. Alternatively also the first nearly flat concentration profile recorded at very short time can be used. If the data are very noisy and additionally the meniscus is not depleted it is of advantage to know the loading concentration and held this parameter constant during the fit. At the begin of the program there is a option to load the 3000 rpm file in the absorption mode to get this information (only for absorption data). Again with the cross hairs the wanted part of the 3000-rpm trace can be determined (pressing key A and E). In the interference mode the program select from the chosen part the important skyline of the trace and subtracted this contour from all data traces.

Additional it is possible to load two data sets with different rotor speeds but identical meniscus, bottom radius and loading concentration. After loading the last data file of

a set you can stop the loading process or you can load one new data set with a new name. The **sedimentation distribution** (see later) $g^*(s)_t$ will be calculated with the first loaded data set alone.

Optional it is possible to correct pull outs by the program by interpolation. This option includes automatically the determination of the last significant data point mentioned below.

The following option enables to determine the last significant data point in the bottom region important for the model function **N**. The last data points can p.e. decrease by technical or optical effects. For other model functions this option is ineffectual.

A special point is the choice of the slit velocity of the XLA. For molecules with quick sedimentation velocity this parameter has some influence especially in the first concentration profiles. The recording time for one trace takes some minutes depending dominantly from the length of the liquid column in the cell and some other parameters p.e. repeat rate by absorption measurements. Accurate details to this problem fail in the XLA-file header or in the manual of the XLA. The program allows to consider or to simulate the influence of this technical parameter. A slit velocity of 0.025 cm/sec is the usual value for radial space of 0.003 cm and no replication of measurements. For smaller space the speed is adequate slower. By input of 'zero slit speed' this correction is switched off. This is automatically done by interference data files.

The program allows to eliminate radial independence errors (**RI-noise**) for all 9 model functions. This means the estimation of local baseline offsets for each data trace.

For **interference** data it is possible to eliminate additionally the time independent (**TI-noise**) errors. For absorption data this is also possible when the option **interpolation of missing** data points was used. Both errors are eliminated according to Schuck and Demeler adapted to our iteration method after Levenberg/Marquardt, which works with derivatives of the model functions in contrast to the method used by Schuck or Demeler. To avoid the linear dependence of the two parameters (TI and RI) contrary to Schuck/Demeler the sum of the local base lines (RI noise) was set to zero. Therefore our procedure allows the use of data sets with different length typical for concentration profiles with higher molecular mass. For **interference data** the subtraction of the sky line (contour) of the 3000 rpm scan is the better method which works with more accuracy (especially at low number of data sets) and moreover somewhat faster. The loading concentration is altered by this procedure and must be estimated as usual.

By use of the model function **N** and **C** up to **four independent species** can be fitted. The start values will be found out by use of the $g^*(s)$ plot (sedimentation coefficient distribution) offered by the program. It can be chosen between radial and time derivative version. The radial version is of advantage when the TI-noise was abolished by the subtraction method. The existence of RI-noise affects then not the quality of the derivative. In the boarder line the following information are given (from left to right). The number of the last file included in the derivative calculation, the intensity of the signal, the Svedberg coefficient both connected with the cross-hairs and the value of radius used in the Bridgman relation, the number of files for averaging, and the file distance used for time derivation. The number of files for averaging can be chosen. By means of the cross-hairs and the number keys (1-4) the peaks (s-values) are selected, the number of independent species is simultaneously determined by this. The starting diffusion coefficients are calculated

from the designated sedimentation coefficients and a supposed friction coefficient of 1.3. By using absorption files it is necessary to use the possibility of interpolation missing data points. The cause is, that the routines used for intensive smoothing the $g^*(s)$ plot presuppose equidistant data points.

Now the program asks for the partial specific volume and the density of the solution to calculate the molecular weight by the Svedberg formula. Additionally the program ask for the friction of the solution to calculate the friction ratio and the stokes radius. As default the friction of water is implemented in the program temperature dependent.

The wanted model function will be select by pressing the designated key. After this the multitude of **not** to estimate parameters is to inspire and then to choice what parameters you mean. This will be done by the number (sequence) of the parameters shown just before separated by space. Instead of the **diffusion** parameter also the **molecular weight** can be given in. The diffusion parameter will then calculated by the program by use of the svedberg equation with the currently estimated sedimentation coefficient. In this case it is also possible to give in additionally the **friction ratio**. The program then calculate the sedimentation and diffusion coefficient by use of the molecular weight, viscosity and specific volume. When the sedimentation parameter is also held constant during the fit only the loading concentration (absorbance) and the meniscus and bottom radius are to estimated. This possibility can be of advantage by fitting more than one independent species for a first attempt. If instead of the **diffusion coefficient** a zero is given in the program ask later for the **friction ratio**. The program held then this ratio constant during the fit and calculates the diffusion coefficient from the current estimated sedimentation coefficient with the help of the given ratio.

Now the program tries to fit the data. The fit progress is shown graphically.

On the bottom of the screen appears a border, which contain 7 numbers.

1. Number of files
2. The square sum of the residuals (SSR)
3. The last improvement of SSR
4. The last improvement of SSR which is necessary to finish the iteration
5. The square sum of the scaled parameter improvements (the solutions of the scaled information matrix) which is additional necessary to finish the iteration
6. The last improvement of this square sum
7. The current damping parameter λ which must be <1 to finish the iteration

On the top of the screen the result of every iteration is given out. The sequence of the parameters is the same as in the parameter input or output (like result printing) and designated by the following letters:

a = amplitude
 s = sedimentation parameter
 z = zero line
 m = meniscus radius
 b = bottom radius
 r = rotation parameter
 D = diffusion parameter
 μ = parameter in $s_c = s_0 - \mu \cdot C / C_{load}$

To avoid endless iterations two other criteria are enclosed. The iteration is also finished either the last improvement of SSR is 0.01 times smaller as mentioned

above or the last improvement of the parameter square sum is 0.1 times smaller as in the triple condition mentioned above (4, 5 and 7).

When the fit is finished, press ESCAPE to continue the program. The fit procedure can alternatively **finished by pressing key 'I'**.

Now the results are shown on the monitor. By use of the function **N** it is taken into account that one restriction holds for the approximate whole boundary solution of the LAMM equation. The solution is composed by two independent solutions consider either meniscus or bottom boundary. This restriction means that meniscus trace and bottom trace should not be influence mutual the corresponding boundary condition markedly. Therefore in the results the actual value of a test parameter is printed out. If this value exceeds the value 1 one or some of the last data sets has to be omitted. The number of the data file, which exceeds firstly the limit value, is also printed out. It is favorable to use high rotor speed (at the same colon length) to obtain lower ε and therefore lower mutual influence.

After showing the values of the estimated parameters the final graphic is presented (press enter). By pressing the keys CRTL+H you can write additionally text horizontally in the graphic beginning at the cross hairs. By pressing the keys CRTL+V this can be done vertically. The graphic can be printed out by **pressing the keys CRTL + L (hard copy)**. In the left corner of the screen are shown (i) the amplifying factor for the residues relative to the concentration profiles and (ii) the OD scale belonging to the two yellow tixes.

After ESCAPE a list of some possibilities (options) is shown. By **pressing the key D** the results will be printed out including the graphic (if CRTL+L was pressed before) and the paper sheet should be ejected. By pressing key **X** only the picture will be printed out. This possibility is of advantage when more than two species are included because the data print plus graphic do then not suit on one page.

A complete output is shown at the begin of this instruction. A file set simulated according to Claverie was fitted with the whole boundary function **N**. The parameter chosen for simulation are shown at the top of the output. The residuals are plotted with 64 fold amplification compared to the data files.

At the end an example for a fit of **4 independent species** is shown together with a hardcopy of the sedimentation distribution plot shown on the screen.

The **option T** represents the possibility to show the two traces, which constitute the whole boundary trace. These two curves are the meniscus part, which represent a Faxen type solution of the Lamm equation, which fulfills the meniscus boundary condition and the bottom part, which fulfills the bottom boundary condition. In the approximate solution used here both curves are taken as independent from another. That means the Faxen solution may be already in the plateau region when the bottom part is already nearly zero.

With the **options S, H and A** it is possible to leave out some data sets from the parameter estimation procedure. The numbers of the files are the numbers on the left hand side of the screen. The option **L** allowed to define a maximal amplitude (OD or fringes) for all date files. Additionally it recommends a maximal amplitude calculated from the greatest slope acceptable for the used model functions **N or R**. With the **option O** all omitted files and data points are restorable.

Additional to the calculation of the mole mass by the Svedberg relation the mass is additionally calculated by the Archibald method. This is done by use of the estimated parameter of the used model function and its differentiated form. Corresponding to

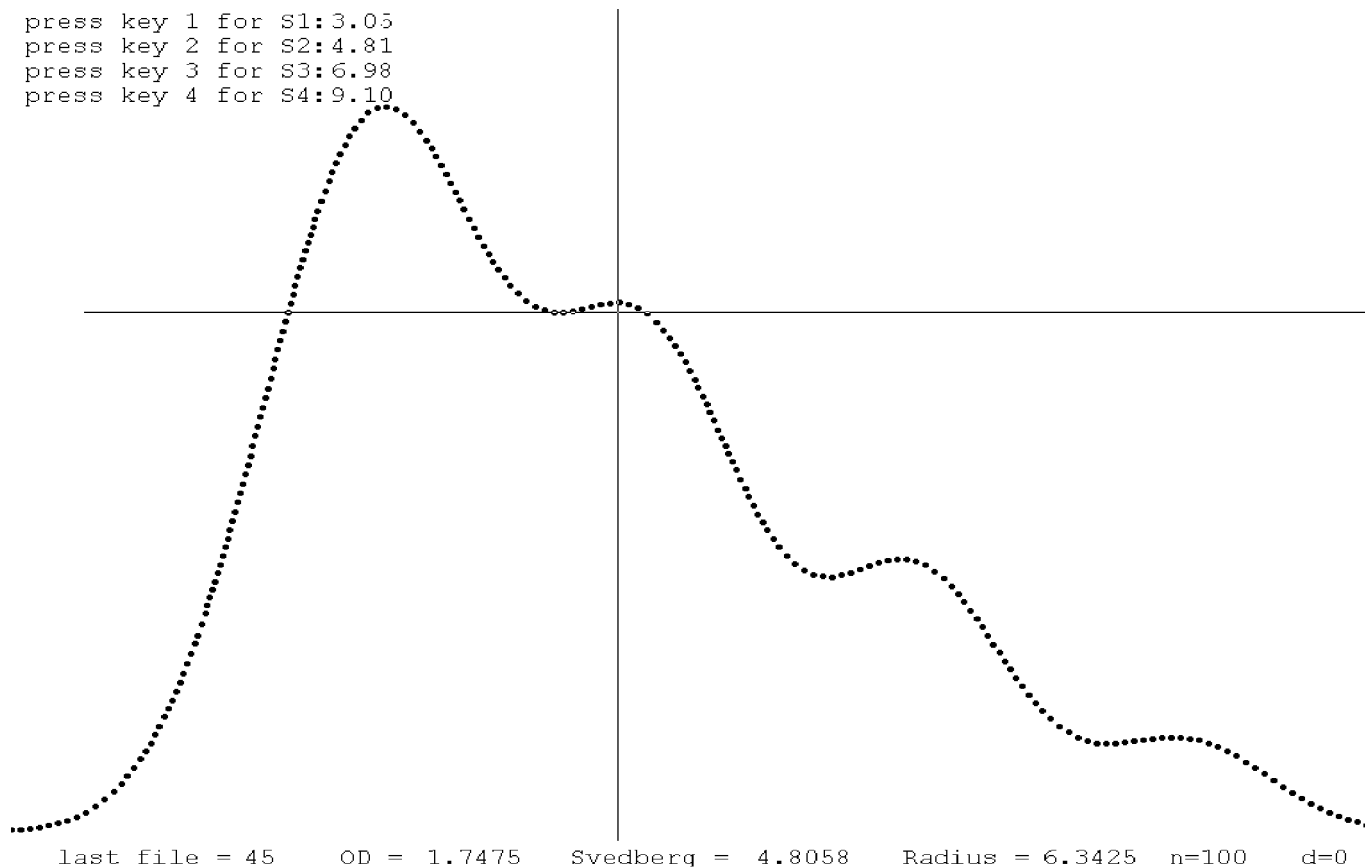
the used model function the Archibald mass is calculated for the meniscus or bottom radius or both but only for the first concentration profile.

The stoke radius and from this the excluded volume are calculated. The friction of the solvent water is taken into account temperature dependent. But the true friction can be given in. Furthermore the friction ratio is calculated.

With the **option U** the sedimentation parameter estimated with the **whole boundary** function **N** can be introduced together with the corresponding data files in the program **SEDFIT** from Schuck. The program LAMM yields the used prepared data files together with two supplement files, the loading list and the starting parameter list for direct loading by SEDFIT. This possibility is valid also for data analyzed with function **C**. In this case the cut up of the data traces to allow faxen type analyze must be done after their completely loading. **LAMM** added the lost data points for use with program SEDFIT. The bottom radius is then the introduced one (with key b). In both cases up to 4 species can be handled. This possibility is valid also for data with nonideal sedimentation analyzed with function **M** but only one species is allowed. When the parameter describing the concentration dependent sedimentation is negative the program interpret this as a rapid monomer-dimer equilibrium. The parameter output is now qualified for the corresponding routine of the program Sedfit (Schuck). The start values are valid when the product of association constant times loading concentration lies in the region $0.1 > Kc < 1$.

The program itself explains many further details.

An additionally possibility is the generation of a graphic (plot) file in the HPGL language (vector graphic) with **option Z**. The position of the plot can be chosen by offset x and y values (in pixels). By choice the additional text in the screen graphic can be drawn within the plot. Additional residual plots can be generated. Up to nine residual plots can be drawn in one picture with four different extensions. The options 'C' and 'G' (gradient curves), residual graphics, RI and TI-noise are also included in this possibility. Each HP-Laser-printer accepts such HGL-files.



Sedimentation distribution plot from the radial derivativ
 according to Bridgman

The left top corner show the from program LAMM accepted s-values
 after pressing the designated keys

The radial differentitation is made with a sliding 53 point parabel
 fitting. The further smoothing also for the time difference method
 takes place again with a sliding 53 point parabel fitting. Number of
 repeats can be chosen (see below).

The bottom border line show from left to right

The file used for the distribution plot, can be chosen by its number

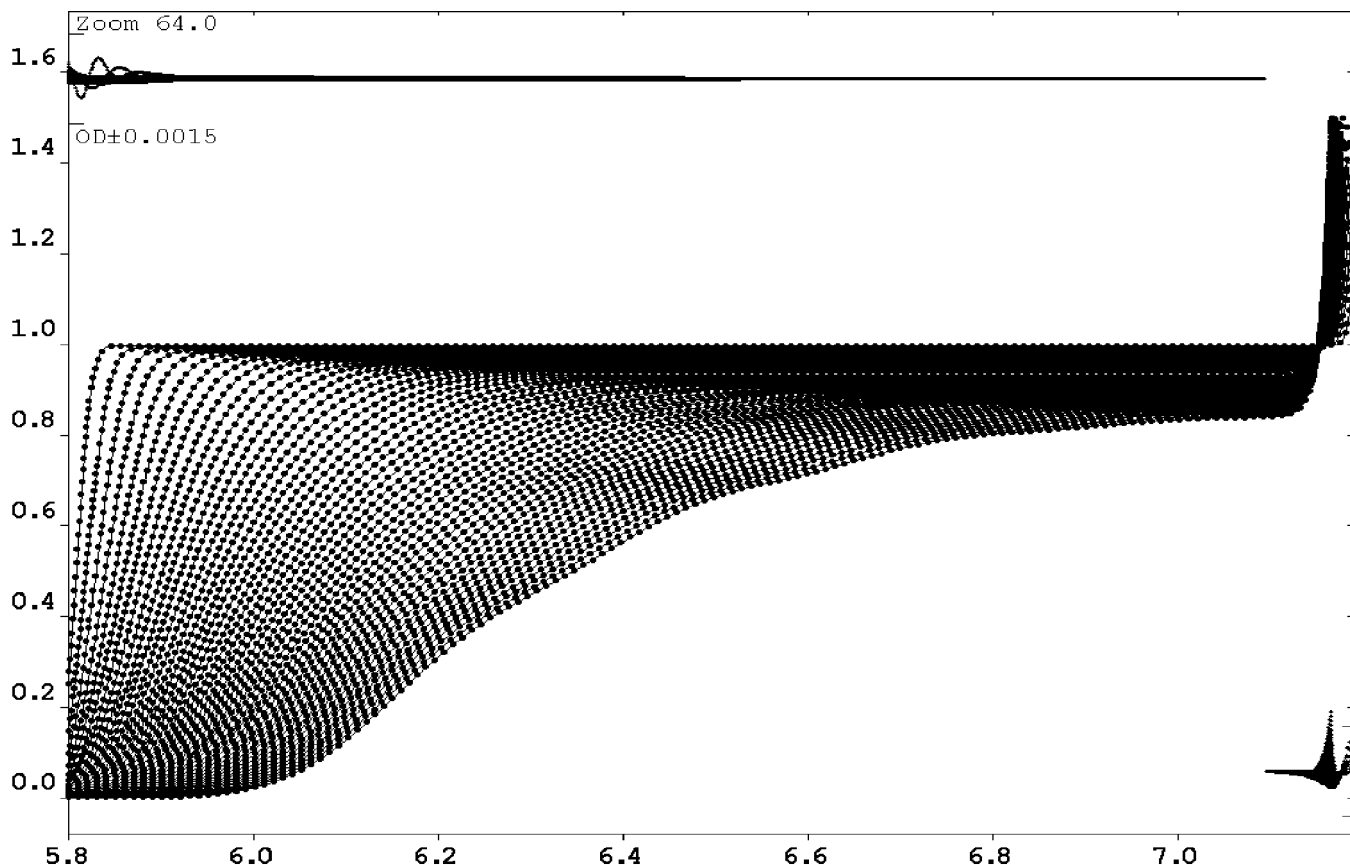
The $g^*(s)$ value in dependence of the horizontal line of cross hairs

The value of sedimentation coefficient in dependence of vertical line

The corresponding radius in the Bridgman relation

The number of repeats for smoothing can be chosen, standard n=100

The two substracted files in the time variant are neighbours, d=1



LAMM (N = correct air + bottom boundary) (absorption) Date: 29:4:2004
 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27
 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50
 Ns:0.000 Amp:0.50 0.30 0.15 0.05 R-Raster:0.0010 T-Raster:1.000 ts: 100
 S=3.00 5.00 7.00 9.00 D=8.438 6.536 5.524 4.872 Rm=5.8 Rb=7.2 td: 100
 C:4param_0

Parameter(total/estimated)/tau(last set)	16/15	1.1840E-01
Data points/files/time offset/TI-noise	68696/ 50 0	FALSE
Cell,temperature,wavelength,rotor:rpm,rpc	9 20.0 220	60000 1
Iterations/faulted/part.spec.vol./load.conc	5/ 0 0.7300	FALSE
Maximal iterations/OD-max/slit speed(mm/sec)	200 1.50	0.0000
Radius range/rpm/Calc. last bottom point	5.8000/7.1950	60000 N
Test for validity<1/no.of data file/RI-noise	0.498 50	FALSE
Cancel outliers/start time(s)/TI-noise subtract. N	100	FALSE
Standard deviation(rmsd)/time diff./SSR	0.00006 100	2.5713E-04
Damping parameter,start / epsilon	0.4938 5.00	4.2482E-03

PARAMETER	VALUE	STD.DEVIATION	START VALUES
Initial absorbance	5.0004E-01	6.1369E-06	4.4014E-01
Svedberg coeff. (Svedb.units)	2.9991E+00	1.5952E-05	3.0209E+00
Base line	-1.5948E-04	9.6247E-07	0.0000E+00
Meniscus radius	5.8000E+00	2.2530E-07	5.8000E+00
Bottom radius	7.2001E+00	2.1958E-07	7.1950E+00
Rotation parameter	0.0000E+00		0.0000E+00
Diffusion coefficient	8.4602E-07	6.7250E-12	7.6523E-07
Molecular mass/stdv/(psv*rho)	3.2010E+04	3.0615E-01	7.3000E-01
Stokes radius(water) (m)/excluded volume(L/g)	2.5159E-09	5.0222E-03	
Water thicknis from stokes radius(m)//-Vol/g	4.1604E-10	5.2554E-01	
Friction ratio/viscosity/rho	1.1981E+00	1.0086E+00	1.0000E+00
2.Initial absorbance	2.9986E-01	8.3275E-06	3.1384E-01
2.Svedberg coeff. (Svedb.units)	4.9983E+00	3.6207E-05	4.9083E+00
2.Diffusion coefficient	6.6053E-07	2.9847E-11	6.0033E-07
Molecular mass/stdv/(psv*rho)	6.8329E+04	3.1270E+00	7.3000E-01
Stokes radius(water) (m)/excluded volume(L/g)	3.2224E-09	4.9435E-03	
Water thicknis from stokes radius(m)//-Vol/g	5.1869E-10	5.0588E-01	
Friction ratio/viscosity/rho	1.1919E+00	1.0086E+00	1.0000E+00

3.Initial absorbance	1.5008E-01	9.0567E-06	1.6492E-01
3.Svedberg coeff.(Svedb.units)	6.9969E+00	6.3369E-05	7.0025E+00
3.Diffusion coefficient	5.6720E-07	6.3364E-11	5.0261E-07
Molecular mass/stdv/(psv*rho)	1.1138E+05	1.2484E+01	7.3000E-01
Stokes radius(water) (m)/excluded volume(L/g)		3.7527E-09	4.7893E-03
Water thicknis from stokes radius(m)//-Vol/g		5.7060E-10	4.6733E-01
Friction ratio/viscosity/rho	1.1793E+00	1.0086E+00	1.0000E+00
4.Initial absorbance	5.0193E-02	6.3742E-06	5.8670E-02
4.Svedberg coeff.(Svedb.units)	8.9961E+00	1.2594E-04	8.9708E+00
4.Diffusion coefficient	5.1494E-07	1.3482E-10	4.4406E-07
Molecular mass/stdv/(psv*rho)	1.5775E+05	4.1361E+01	7.3000E-01
Stokes radius(water) (m)/excluded volume(L/g)		4.1335E-09	4.5194E-03
Water thicknis from stokes radius(m)//-Vol/g		5.6007E-10	3.9985E-01
Friction ratio/viscosity/rho	1.1567E+00	1.0086E+00	1.0000E+00